

IMPROVEMENTS RELATING TO CONTACT-LESS POWER TRANSFER

This invention relates to a new device for transferring power in a contact-less fashion, for example electromagnetic induction.

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Today's inductively-chargeable portable devices, for example the Braun Oral B Plak Control power toothbrush, must typically be precisely aligned with their charger in order to charge them. This precision is necessary so that the coil in the device is correctly aligned with the coil in the charger – the coils being, in effect, the two halves of a conventional power transformer.

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Some examples of typical prior art are shown in Figure 1. In Figure 1a, the primary coil of the charger is aligned with the secondary coil of the device. In Figure 1b, a horseshoe electromagnet on the charger is aligned with a similar electromagnet on the device. Figure 1c operates in a very similar way to Figure 1b: the field is created by two coils operating in antiphase (with the lower return circuit being an air gap), and the secondary coil is a flat wound coil. Prior art such as US4873677 works in such a fashion. Note in all cases the precise alignment that is required in order to achieve good coupling between the primary and secondary coils.

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Referring now to Figure 2 which explains some terminology used in the present application: Figure 2a shows some charger 201 with a surface 203, the charger 201 emitting a field, and some device 202 charging from the charger 201 (and appreciating that in this figure the shapes of both are irrelevant). Figure 2b shows that the device 202 may move about on ("be translated relative to") the surface 203 of the charger 201 in two directions, depicted X and Y, which are at right angles to one another. The device 202 may also move nearer to and further from the charger 201 in direction Z, but as this will eventually take it out of the charging field, and this is therefore not considered here.

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Figure 2c shows that in addition to the above translations, the device 202 may rotate around the X axis (rX), the Y axis (rY) and the Z axis (rZ). In the present application,

only rotations about rZ, and not those around rX or rY, shall be considered. Each of these six translations and rotations is independent from (also known as “orthogonal to”) the others, and is known as a “degree of freedom”.

- 5 Figure 2d shows an alternative translation co-ordinate system. Instead of orthogonal (X,Y) movement, the position of the device 202 is determined by the radius (r) and the angle (θ) from some centre point. Even though θ involves rotation, it is still a translational degree of freedom, since the device 202 itself need not rotate about its own axis.

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For maximum user convenience a system should allow up to five degrees of freedom - translation in the Z axis not being of practical use - so that a device 202 can be placed without regard to its position or orientation on the charger 201.

- 15 But today's toothbrush chargers and the like are typically much more constrained. Systems employing the transformer configuration shown in Figure 1a offer one degree of freedom (rotation in the plane of the coils), and those shown in Figure 1b and Figure 1c offer zero degrees of freedom, since if the device is to continue to receive adequate power it cannot be either rotated nor translated relative to the
20 charger. Having zero - or only a few - degrees of freedom requires precise alignment which may be inconvenient to the user because it requires a degree of care and manual dexterity in placing the device 202 on the charger 201.

- In addition, systems lacking the translational (X and Y) degrees of freedom cannot
25 charge multiple devices simultaneously, because of course not more than one device can occupy the required (X,Y) position at once.

- In addition, such systems requiring precise primary:secondary alignment are also not
a universal inductive charging solution – one able to charge devices with very
30 different power requirements – because the different coil sizes mandated by the power needs of different types of devices will not be a good match for any single size of charger coil – see Figure 3.

Various means of increasing the number of degrees of freedom have been proposed.

One simple method is to have a large coil in the charger, emitting a large field,
5 allowing the device to pick-up sufficient power even if it is not perfectly aligned.
Figure 4, for example, shows such a charger coil 401 and device coil 402. This is the
method adopted by various RFID devices. However the coupling between the coils
401 and 402 will be poor and highly variable dependent on position, so this solution
is inefficient and limits the power that can be transferred while still complying with
10 emission legislation. Therefore this solution is far from ideal in charging
applications, where efficiency is typically an important criterion.

A solution which improves upon the efficiency of such “large coil” systems, while
still offering several degrees of freedom, is to use multiple coils in the charger,
15 enabled as appropriate, ensuring that there is always a reasonable match between
nearby charger coils and the device coil. See Figure 5, showing multiple charger
coils 501 and single device coil 502. Prior art includes:

- A system is described in the Journal of the Magnetics Society of Japan titled
20 “Coil Shape in a Desk-type Contactless Power Station System” (29th Nov
2001)

An alternative solution is the present applicant's UK patent application number
0210886.8 of 13 May 2002, which discloses a system generating a horizontal field
across the surface of the charger, in contrast to conventional solutions which generate
25 a vertical field out of the surface of the charger. A copy of equivalent International
patent application no PCT/GB2003/002030 is being filed with the present application
so as to form part of the file thereof, and the full contents of PCT/GB2003/002030
are hereby incorporated into the present application by reference. This offers the
same two translational degrees of freedom (X and Y) as the above multiple-coil
30 approach, but with better field uniformity and therefore worst-case efficiency.
Optionally, the horizontal field may be rotated in the plane of the charger, offering an
additional one degree of rotational freedom (rZ). See Figure 6 which shows a laminar

charger 601 generating a magnetic field in the plane of the charger 602 and a device 610 capable of receiving power from such a field when it is in a certain alignment 611. If the field generated by the charger is made to rotate, as shown, then there is no requirement to align the device in any particular orientation.

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According to a first aspect of the present invention, there is provided a unit for transferring power in an inductive manner to at least one power-receiving device, the unit being provided with at least one electrical coil, and the power-receiving device being capable of receiving power when placed in more than one position or rotation
10 on the unit.

The unit may include a pad in which the coils are disposed, the pad serving as a surface upon which power-receiving devices may be placed in order to effect power transfer. The unit may incorporate a power supply or be connectable to a power
15 supply. The pad is preferably a laminar pad, i.e. has a configuration of a lamina. In other words, the pad is preferably generally flat, and may be substantially planar, it being understood that the pad may take a curved form or be made conformal to a curved surface such as the inside of a glove compartment in an automobile. This may apply also to the further aspects of the invention set out hereinbelow.

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According to a second aspect of the present invention, there is provided a unit for transferring power in an inductive manner to at least one power-receiving device, the unit being provided with a plurality of electrical coils, the electrical coils not all
25 being of the same shape.

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The coils may be simple conductive loops, or may comprise a more complex arrangement of conductors. Where a more complex arrangement of conductors is provided, for example as disclosed in the present applicant's co-pending UK patent applications numbers 0210886.8 of 13th May 2002 and 0213024.3 of 7th June 2002
30 (the full disclosures of which are hereby incorporated into the present application by reference), the term "coil" in the context of the present application is intended to denote each separate arrangement of conductors that defines a given charging region

or active area on the primary unit and on which a secondary device is placed in order to effect charging.

5 The plurality of electrical coils preferably in this aspect may also not all be of the same size and/or not all enclose the same dimensional area.

According to a third aspect of the present invention, there is provided a unit for transferring power in an inductive manner to at least one power-receiving device, the unit being provided with a plurality of electrical coils, the electrical coils not all
10 being of the same size and/or not all enclosing the same dimensional area.

In some embodiments, all the coils may be of mutually different shapes and/or sizes and/or dimensional areas. In other embodiments, two or more of the plurality of coils may have the same shape and/or size and/or dimensional area, with the
15 remaining coils having one or more different shapes and/or sizes and/or dimensional areas, or all having the same different shape and/or size and/or dimensional area.

The coils may be spatially separated from each other such that no coil is enclosed in or overlaps with any other coil. Alternatively, one or more smaller coils may be
20 contained within a boundary of one or more larger coils. Where one or more smaller coils are contained within a boundary of a larger coil, the coils may be substantially concentric, or may have some other arrangement. For example, a plurality of smaller coils may be contained within a boundary of a larger coil in such a way that the smaller coils are not contained within each other or overlap with each other. Some
25 smaller coils may be nested within each other within the boundary of a larger coil, with some other smaller coils not being nested within each other within the same outer boundary.

The coils may take various shapes, including circular, elliptical, generally ovate,
30 triangular, rectangular, parallelogram, trapezoidal, star-shaped, regular polygonal, irregular polygonal or amorphous.

According to a fourth aspect of the present invention, there is provided a unit for transferring power in an inductive manner to at least one power-receiving device, the unit being provided with at least one plurality of nested electrical coils and also with means for selectively activating one or more of the nested electrical coils so as to be adaptable to provide efficient power transfer to power-receiving devices of different sizes and/or power requirements and/or positions/rotations.

The means for selectively activating one or more of the nested coils may be adapted automatically to sense an appropriate size and/or power requirement and/or position/rotation determinant of the power-receiving unit (for example, a size or sizes of secondary power-receiving coils in the power-receiving device).

The nested coils may be substantially circular, or may take any other appropriate shape as outlined above.

In a particularly preferred embodiment, there are provided four nested sets of electrical coils, each having a substantially right-angled triangular shape, and arranged such that the right-angles of the four sets of coils all point towards a single origin point such that the four sets of nested coils have an overall substantially square or rectangular configuration. Preferably, adjacent sets of coils are driven in antiphase so as to cause rotation of a resultant electromagnetic field about the origin point, thereby providing a degree of rotational freedom in the positioning of a power-receiving device on the pad.

According to a fifth aspect of the present invention, there is provided a unit for transferring power in an inductive manner to at least one power-receiving device, the unit being provided with an even number of electrical coils each having corner portion, the coils being arranged such that the corner portions all point towards an origin point, and wherein, in operation, adjacent coils are driven in antiphase so as to cause rotation of a resulting electromagnetic field about the origin point.

There is preferably provided four coils, which may each have a substantially right-angled triangle shape, a quarter circular shape or any other appropriate shape. Where more than four coils are provided, they may each have a generally triangular shape or take the shape of a sector of a circle.

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Any of the first to fourth aspects of the present invention may be combined with at least one power-receiving unit so as to form a system for contact-less power transfer.

10 According to a sixth aspect of the present invention, there is provided a system for contact-less power transfer, the system comprising a power-transmitting unit provided with a primary coil and at least one power-receiving device incorporating a secondary coil, wherein the primary coil is generally elongate along an x-axis with respect to an orthogonal y-axis, and wherein the secondary coil is sized so as to be sufficiently similar in size to the primary coil with respect to the y-axis so as to
15 provide efficient power transfer, but smaller in size with respect to the x-axis so as to provide a translational degree of freedom of movement along the x-axis.

In this way, several power-receiving devices may be simultaneously provided with power by the primary coil by placing the devices adjacent each other along the x-
20 axis.

The primary coil may be generally rectangular, or any other appropriate shape, including elliptical or generally ovate. The secondary coil preferably has a corresponding rectangular (possibly square) or elliptical or ovate or other
25 configuration, subject to the constraints that the extent of the primary coil along the y-axis is substantially similar to that of the secondary coil along the y-axis, and that the extent of the primary coil along the x-axis is greater than that of the secondary coil along the x-axis. Preferably, the extent of the primary coil along the x-axis is at least twice, advantageously at least three or four times, that of the secondary coil
30 along the x-axis.

According to a seventh aspect of the present invention, there is provided a system for contact-less power transfer, the system comprising a power-transmitting unit provided with at least one primary coil having a boundary portion and at least one power-receiving device incorporating a secondary coil, wherein power transfer takes place by way of coupling of near-field flux flowing about the boundary portion of the at least one primary coil with windings of the secondary coil.

There may be provided just a single primary coil of appropriate configuration, or a plurality of adjacent primary coils which will enable a plurality of power-receiving devices to receive power simultaneously.

The at least one primary coil may be generally rectangular in shape, in which case there is one linear degree of freedom of movement of the secondary coil.

Alternatively, the at least one primary coil may be substantially circular or elliptical or the like, in which case a rotational degree of freedom of movement is provided.

According to an eighth aspect of the present invention, there is provided a system for contact-less power transfer, the system comprising a power-transmitting unit provided with first and second substantially concentric primary coils, the first being larger than the second, and at least one power-receiving device incorporating at least one secondary coil dimensioned so as to correspond to a distance between the first and second primary coils, wherein power transfer takes place by way of coupling of near-field flux flowing about the boundaries of the first and second primary coils with generally opposed edges of the secondary coil.

The first and second primary coils in this aspect are supplied with currents flowing in opposite directions. The coils may be generally circular, or may take any other appropriate shape as hereinbefore described.

Summarising the above, the table below lists the desirable characteristics of any inductive charging system, and illustrates how those of the present invention compare with prior art:

	<u>Today's chargers</u>	<u>Present invention</u>	<u>UK 0210886.8</u>
<u>Simple</u> <i>(therefore cheap to make)</i>	<u>Y</u>	<u>Y</u>	<u>Y</u>
<u>Efficient and uniform field</u> <i>(high-power within regulations)</i>	<u>Y</u>	<u>Y</u>	<u>Y</u>
<u>Simultaneous</u> <i>(more than one device at a time)</i>	<u>N</u>	<u>Y</u>	<u>Y</u>
<u>Universal</u> <i>(many types of devices)</i>	<u>N</u>	<u>Y</u>	<u>Y</u>
<u>Degrees of freedom</u> <i>(convenience)</i>	<u>0 or 1 (rZ)</u>	<u>0..2 of (X,Y,rZ)</u>	<u>2 (X,Y) 3 (X,Y, rZ)</u>

5 Embodiments of the present invention may therefore provide greater simplicity (and thus reduced cost) by offering a number of degrees of freedom which is less than that of GB 0210886.8, but greater than that of today's "toothbrush" chargers, while still preserving many of the benefits of GB 0210886.8 (Simplicity, Efficiency, Simultaneity and Universality).

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Additionally, this may optionally be achieved while still retaining forward compatibility with devices and chargers of the type described in GB 0210886.8.

15 There shall now be described various embodiments of the present invention that fit into the following three categories:

1. No degrees of freedom – the charger has different positions for different types of device (Figure 7)
2. Only the rZ rotational degree of freedom, so the device has to be placed in the correct position on the charger. The charger has a single location with an effective coil size that alters with device needs (Figure 8 and Figure 9)

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3. Only one translational degree of freedom (Figure 10), either:

- a. Linear translational
- b. Circular translational, and rotational

5 Addressing each of these categories in turn:

1. No degrees of freedom

Figures 7a,7b,7c show three different types of charger configuration 701 which each have several sizes or shapes of coil 702,703,704. Each coil could be, for example, a multiply-wound coil of a type similar to that in Figure 1a. The coils may all be driven simultaneously, or only when a device is sensed.

The location and/or rotation and/or type of each coil is made clear by some indicator, allowing the user to place their device onto the coil which best couples to it, and in the correct orientation if such is necessary.

In Figure 7a, the coils are spatially separate (allowing multiple devices to be charged simultaneously), in Figure 7b they are concentric, and in Figure 7c they are a mixture of the two.

The coils can of course be of any shape to suit the device, and some examples are shown in Figure 7d.

2. Only the one rZ rotational degree of freedom

Figures 1a and 8a show a prior art system with a single rotational degree of freedom – a coil on the primary 800 couples to a corresponding coil on the device 801 in the manner of a simple transformer.

Figure 8b shows an alternative method of achieving the same rotational degree of freedom for a device 811 which expects a field in the manner of Figure 1c. An antiphase field is driven into sets of coils 810A and 810B such that the field rotates from being aligned in the 810A axis to being aligned in the 810B axis and back to

810A. Thus over time the device receives a significant amount of power no matter what its orientation.

Figure 9 extends these two means of generating a rotational degree of freedom by adding universality. A charger 901 consists of a number of such coils, arranged concentrically, each of which can be driven independently. The charger behaves differently depending on which type of device is present 902.

- In Figure 9a no device is present, and so no charger coils are driven.
- In Figure 9b a physically small device with correspondingly small power requirements is present, and so only a few of the inner coils are driven.
- In Figure 9c a physically large device with correspondingly large power requirements is present, and so many of the coils are driven.

Figures 9d,9e,9f show a charger with a coil configuration 903 of the type shown in Figure 8b, but again arranged concentrically as above, with similar benefits.

3a. One linear translational degree of freedom

Figure 10 shows various configurations in which the primary charger coil is larger than the secondary device coil, but constrained in its dimensions such that it offers a reasonably efficiency with a single translational degree of freedom in the X axis, and therefore the option of simultaneous charging of multiple devices.

In Figure 10a a rectangular charger coil 1001 drives a smaller device coil 1002 by generating a field in the Z axis. By being similar in size to the device coil in the Y dimension, reasonable efficiency is obtained. By being significantly larger than the device coil in the X dimension, one degree of translational freedom is achieved.

Of course the coils could be any type of shape (for example ellipsoidal) rather than rectangular as shown – an important point is the aspect ratio.

Figures 10b and 10c achieve a similar result for devices of the Figure 1c type, 1003. In Figure 10b, a charger coil identical to Figure 10a is used. In Figure 10a it was be

considered to be generating a net flux out from the centre of the coil in the Z dimension, but it can equally be viewed “up close” to the edge of the coil as generating a flux which is rotating around the wire(s), as shown in Figure 10b. Therefore if a device of Figure 1c is placed across any edge of the coil, it will receive the flux,

In Figure 10c a second coil is placed below the first 1004. If placed along the boundary between the two, as shown, the device coil will receive power from each coil. Of course this concept can be extended indefinitely in the Y dimension, as shown with a dotted line, to produce any number of lines along which a device may receive power.

3b. One circular translational degree of freedom

Figure 11a shows a large coil 1101 with a small coil 1102 inside it. The coils carry current in opposite directions, and so will generate a net flux flowing in the Z axis (out of the page). If a device with a coil 1103 is placed anywhere within the annulus formed between the coils, it will receive this flux with reasonable efficiency. Thus the device has a circular translational degree of freedom, and multiple devices can be placed on the charger.

Figure 11b shows a similar scheme working with a device of Figure 1c type. The device straddles the outer coil 1101 to couple with it. This could be seen as a variant of Figure 10b.

It will be appreciated that the coils do not have to be circular.

In each of the above cases, the charger may sense if any device is present on any particular coil, and if so what its power needs are. Possible means for doing this include but are not limited to:

- Sensing the resonance (“Q”) or other characteristics of the driven coils
- Communication by modulation of data signals onto the magnetic field (e.g. “back-scatter”, as used by RFID devices).

In all embodiments of this present application, the user has limited degrees of freedom when placing devices. Therefore it may be advantageous to indicate these constraints to the user.

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Such indications may be done in a variety of ways, for example:

- For chargers with placement restrictions, indicating the correct device position by means of:
 - Outlining of the coil area
 - Filling, or patterning, the active coil area.
- For chargers with rotational restrictions, indicating the correct device rotation by means of:
 - A line or arrow, or set of such.

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15 The indications may be rendered in any number of media, for example:

- Printing ink, perhaps of a particular colour
- Raising or lowering the charger surface.
- Overall shape of the charger, or part of it.

20 The device may include corresponding indications.

Some examples of possible indications are shown in Figure 12, which:

- Figure 12a shows a printed or raised outline of two devices, for chargers which have no degrees of freedom.
- Figure 12b shows a printed or raised arrow on both the charger and the device, for chargers with 2 translational but not rotational degrees of freedom.
- Figure 12c shows similar to 12b, but with striped indication instead of arrows.
- Figure 12d shows a “target” of concentric circles on both charger and device, for chargers with only a rotational degree of freedom.
- Figure 12e shows a charger with one circular translational degree of freedom, designed such that the active area of the charger is obvious from its form.

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Prior art such as US5952814 [Philips phone charger with interlock] describes how the casing of charger may be made to match the internal shape of the charger thus allowing for accurate alignment of the primary and secondary coils.

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It will be appreciated that in the case of a device coil designed to receive power by picking-up flux travelling substantially in the plane of the charger, as opposed to orthogonal to it, numerous possible designs of core are possible, for example but not limited to:

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- a rod of permeable material with wire coiled around it (Figure 13a) or
- a flat piece of permeable material with a wire coiled flat around it (Figure 13b), as in Figure 1c.

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It will also be appreciated that in any of the above, the precise shape of any coils in the device and/or charger will have an effect on the efficiency and other characteristics. For example, replacing any square coil with a circular coil may reduce efficiency somewhat, but, thanks to the rotational symmetry of a circle, allows the device to have a rotational degree of freedom.

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The preferred features of the invention are applicable to all aspects of the invention and may be used in any possible combination.

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Throughout the description and claims of this specification, the words "comprise" and "contain" and variations of the words, for example "comprising" and "comprises", mean "including but not limited to", and are not intended to (and do not) exclude other components, integers, moieties, additives or steps.

IMPROVEMENTS RELATING TO CONTACT-LESS POWER TRANSFER

The present application claims priority from UK patent applications nos 0210886.8 of 13th May 2002, 0213024.3 of 7th June 2002, 0225006.6 of 28th October 2002 and
5 0228425.5 of 6th December 2002, as well as from US patent application no 10/326,571 of 20th December 2002. The full contents of all of these prior patent applications is hereby incorporated into the present application by reference.

This invention relates to a new apparatus and method for transferring power in a
10 contact-less fashion.

Many of today's portable devices incorporate "secondary" power cells which can be recharged, saving the user the cost and inconvenience of regularly having to purchase new cells. Example devices include cellular telephones, laptop computers, the Palm
15 500 series of Personal Digital Assistants, electric shavers and electric toothbrushes. In some of these devices, the cells are recharged via inductive coupling rather than direct electrical connection. Examples include the Braun Oral B Plak Control power toothbrush, the Panasonic Digital Cordless Phone Solution KX-PH15AL and the Panasonic multi-head men's shavers ES70/40 series.

20 Each of these devices typically has an adaptor or charger which takes power from mains electricity, a car cigarette lighter or other sources of power and converts it into a form suitable for charging the secondary cells. There are a number of problems associated with conventional means of powering or charging these devices:

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- Both the characteristics of the cells within each device and the means of connecting to them vary considerably from manufacturer to manufacturer, and from device to device. Therefore users who own several such devices must also own several different adaptors. If users are going away on travel,
30 they will have to bring their collection of chargers if they expect to use their devices during this time.

5 •—These adaptors and chargers often require users to plug a small connector into the device or to place the device with accurate alignment into a stand causing inconvenience. If users fail to plug or place their device into a charger and it runs out of power, the device becomes useless and important data stored locally in the device might even be lost.

10 •—In addition, most adaptors and chargers have to be plugged into mains sockets and hence if several are used together, they take up space in plug strips and create a messy and confusing tangle of wires.

15 •—Besides the above problems with conventional methods of recharging devices, there are also practical problems associated with devices having an open electrical contact. For example, devices cannot be used in wet environments due to the possibility of corroding or shorting out the contacts and also they cannot be used in flammable gaseous environments due to the possibility of creating electrical sparks.

20 Chargers which use inductive charging remove the need to have open electrical contacts hence allowing the adaptor and device to be sealed and used in wet environments (for example the electric toothbrush as mentioned above is designed to be used in a bathroom). However such chargers still suffer from all other problems as described above. For example, the devices still need to be placed accurately into a charger such that the device and the charger are in a predefined relative position (See Figures 1a and 1b). The adaptors are still only designed specifically for a certain make and model of device and are still only capable of charging one device at a time.

25 As a result, users still need to possess and manage a collection of different adaptors.

30 Universal chargers (such as the Maha MH-C777 Plus Universal charger) also exist such that battery packs of different shapes and characteristics can be removed from the device and charged using a single device. Whilst these universal chargers eliminate the need for having different chargers for different devices, they create even more inconvenience for the user in the sense that the battery packs first need to

be removed, then the charger needs to be adjusted and the battery pack needs to be accurately positioned in or relative to the charger. In addition, time must be spent to determine the correct pair of battery pack metal contacts which the charger must use.

5 It is known from US 3,938,018 "Induction charging system" to provide a means for non-contact battery charging whereby an inductive coil on the primary side aligns with a horizontal inductive coil on a secondary device when the device is placed into a cavity on the primary side. The cavity ensures the relatively precise alignment which is necessary with this design to ensure that good coupling is achieved between
10 the primary and secondary coils.

It is also known from US 5,959,433 "Universal Inductive Battery Charger System" to provide a non-contact battery charging system. The battery charger described includes a single charging coil which creates magnetic flux lines which will induce
15 an electrical current in a battery pack which may belong to cellular phones or laptop computers.

It is also known from US 4,873,677 "Charging Apparatus for an Electronic Device" to provide an apparatus for charging an electronic device which includes a pair of
20 coils. This pair of coils is designed to operate in anti-phase such that magnetic flux lines are coupled from one coil to the other. An electronic device such as a watch can be placed on these two coils to receive power.

It is also known from US 5,952,814 "Induction charging apparatus and an electronic
25 device" to provide an induction charger for charging a rechargeable battery. The shape of the external casing of the electronic device matches the internal shape of the charger thus allowing for accurate alignment of the primary and secondary coils.

It is also known from US 6,208,115 "Battery substitute pack" to provide a substitute
30 battery pack which may be inductively recharged.

It is known from WO 00/61400 "Device for Inductively Transmitting Electrical Power" to provide a means of transferring power inductively to conveyors.

5 It is known from WO 95/11545 "Inductive power pick up coils" to provide a system for inductive powering of electric vehicles from a series of in-road flat primaries.

To overcome the limitations of inductive power transfer systems which require that secondary devices be axially aligned with the primary unit, one might propose that an obvious solution is to use a simple inductive power transfer system whereby the primary unit is capable of emitting an electromagnetic field over a large area (See Figure 2a). Users can simply place one or more devices to be recharged within range of the primary unit, with no requirement to place them accurately. For example this primary unit may consist of a coil encircling a large area. When a current flows through the coil, an electromagnetic field extending over a large area is created and devices can be placed anywhere within this area. Although theoretically feasible, this method suffers from a number of drawbacks. Firstly, the intensity of electromagnetic emissions is governed by regulatory limits. This means that this method can only support power transfer at a limited rate. In addition, there are many objects that can be affected by the presence of an intense magnetic field. For example, data stored on credit cards may be destroyed and objects made of metal will have induced therein eddy currents generating undesired heating effects. In addition, if a secondary device comprising a conventional coil (see Figure 2a) is placed against a metallic plate such as a copper plane in a printed circuit board or metallic can of a cell, coupling is likely to be significantly reduced.

25 To avoid the generation of large magnetic fields, one might suggest using an array of coils (See Figure 3) whereby only the coils needed are activated. This method is described in a paper published in the Journal of the Magnetism Society of Japan titled "Coil Shape in a Desk-type Contactless Power Station System" (29th Nov 2001). In an embodiment of the multiple-coil concept, a sensing mechanism senses the relative location of the secondary device relative to the primary unit. A control system then activates the appropriate coils to deliver power to the secondary device in a localised

- fashion. Although this method provides a solution to the problems previously listed, it does so in a complicated and costly way. The degree to which the primary field can be localised is limited by the number of coils and hence the number of driving circuits used (i.e. the "resolution" of the primary unit). The cost associated with a multiple coil system would severely limit the commercial applications of this concept. Non-uniform field distribution is also a drawback. When all the coils are activated in the primary unit, they sum to an equivalent of a large coil, the magnetic field distribution of which is seen to exhibit a minimum at the centre of the coil.
- Another scheme is outlined in US 5,519,262 "Near Field Power Coupling System", whereby a primary unit has a number of narrow inductive coils (or alternatively capacitive plates) arranged from one end to the other of a flat plate, creating a number of vertical fields which are driven in a phase-shifted manner so that a sinusoidal wave of activity moves across the plate. A receiving device has two vertical field pickups arranged so that regardless of its position on the plate it can always collect power from at least one pickup. While this scheme also offers freedom of movement of the device, it has the disadvantages of needing a complex secondary device, having a fixed resolution, and having poor coupling because the return flux path is through air.
- None of the prior art solutions can satisfactorily address all of the problems that have been described. It would be convenient to have a solution which is capable of transferring power to portable devices with all of the following features and is cost effective to implement:
- Universality: a single primary unit which can supply power to different secondary devices with different power requirements thereby eliminating the need for a collection of different adaptors and chargers;
 - Convenience: a single primary unit which allows secondary devices to be placed anywhere within an active vicinity thereby eliminating the need for plugging in or placing secondary devices accurately relative to an adaptor or charger;

- Multiple-load: a single primary unit that can supply power to a number of secondary different devices with different power requirements at the same time;
- 5 • Flexibility for use in different environments: a single primary unit that can supply power to secondary devices such that no direct electrical contact is required thereby allowing for secondary devices and the primary unit itself to be used in wet, gaseous, clean and other atypical environments;
- 10 • Low electromagnetic emissions: a primary unit that can deliver power in a manner that will minimize the intensity and size of the magnetic field generated.

It is further to be appreciated that portable appliances are proliferating and they all need batteries to power them. Primary cells, or batteries of them, must be disposed of once used, which is expensive and environmentally unfriendly. Secondary cells or
15 batteries can be recharged and used again and again.

Many portable devices have receptacles for cells of an industry standard size and voltage, such as AA, AAA, C, D and PP3. This leaves the user free to choose whether to use primary or secondary cells, and of various types. Once depleted,
20 secondary cells must typically be removed from the device and placed into a separate recharging unit. Alternatively, some portable devices do have recharging circuitry built in, allowing cells to be recharged in situ once the device is plugged in to an external source of power.

25 It is inconvenient for the user to have to either remove cells from the device for recharging, or to have to plug the device into an external power source for recharging in situ. It would be far preferable to be able to recharge the cells without doing either, by some non-contact means.

30 Some portable devices are capable of receiving power coupled inductively from a recharger, for example the Braun Oral B Plak Control toothbrush. Such portable devices typically have a custom, dedicated power receiving module built in to the

device, which then interfaces with an internal standard cell or battery (which may or may not be removable);

5 However it would be convenient if the user could transform any portable device which accepts industry standard cell sizes into an inductively rechargeable device, simply by fitting inductively rechargeable cells or batteries, which could then be recharged in situ by placing the device onto an inductive recharger.

10 Examples of prior art include US 6,208,115, which discloses a substitute battery pack which may be inductively recharged.

According to a first aspect of the present invention, there is provided a system for transferring power without requiring direct electrical conductive contacts, the system comprising:

15 i) — a primary unit including a substantially laminar charging surface and at least one means for generating an electromagnetic field, the means being distributed in two dimensions across a predetermined area in or parallel to the charging surface so as to define at least one charging area of the charging surface that is substantially
20 coextensive with the predetermined area, the charging area having a width and a length on the charging surface, wherein the means is configured such that, when a predetermined current is supplied thereto and the primary unit is effectively in electromagnetic isolation, an electromagnetic field generated by the means has electromagnetic field lines that, when averaged over any quarter length part of the
25 charging area measured parallel to a direction of the field lines, subtend an angle of 45° or less to the charging surface in proximity thereto and are distributed in two dimensions thereover, and wherein the means has a height measured substantially perpendicular to the charging area that is less than either of the width or the length of the charging area; and

30 ii) — at least one secondary device including at least one electrical conductor;

wherein, when the at least one secondary device is placed on or in proximity to a charging area of the primary unit, the electromagnetic field lines couple with the at least one conductor of the at least one secondary device and induce a current to flow therein.

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According to a second aspect of the present invention, there is provided a primary unit for transferring power without requiring direct electrical conductive contacts, the primary unit including a substantially laminar charging surface and at least one means for generating an electromagnetic field, the means being distributed in two dimensions across a predetermined area in or parallel to the charging surface so as to define at least one charging area of the charging surface that is substantially coextensive with the predetermined area, the charging area having a width and a length on the charging surface, wherein the means is configured such that, when a predetermined current is supplied thereto and the primary unit is effectively in electromagnetic isolation, an electromagnetic field generated by the means has electromagnetic field lines that, when averaged over any quarter length part of the charging area measured parallel to a direction of the field lines, subtend an angle of 45° or less to the charging surface in proximity thereto and are distributed in two dimensions thereover, and wherein the means has a height measured substantially perpendicular to the charging area that is less than either of the width or the length of the charging area.

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According to a third aspect of the present invention, there is provided a method of transferring power in a non conductive manner from a primary unit to a secondary device, the primary unit including a substantially laminar charging surface and at least one means for generating an electromagnetic field, the means being distributed in two dimensions across a predetermined area in or parallel to the charging surface so as to define at least one charging area of the charging surface that is substantially coextensive with the predetermined area, the charging area having a width and a length on the charging surface, the means having a height measured substantially perpendicular to the charging area that is less than either of the width or the length of

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the charging area, and the secondary device having at least one electrical conductor;
wherein:

5 i) ~~an electromagnetic field, generated by the means when energised with a predetermined current and measured when the primary unit is effectively in electromagnetic isolation, has electromagnetic field lines that, when averaged over any quarter length part of the charging area measured parallel to a direction of the field lines, subtend an angle of 45° or less to the charging surface in proximity thereto and are distributed in two dimensions over the at least one charging area~~
10 ~~when averaged thereover; and~~

ii) ~~the electromagnetic field links with the conductor of the secondary device when this is placed on or in proximity to the charging area.~~

15 ~~According to a fourth aspect of the present invention, there is provided a secondary device for use with the system, unit or method of the first, second or third aspects, the secondary device including at least one electrical conductor and having a substantially laminar form factor.~~

20 ~~In the context of the present application, the word “laminar” defines a geometry in the form of a thin sheet or lamina. The thin sheet or lamina may be substantially flat, or may be curved.~~

~~The primary unit may include an integral power supply for the at least one means for~~
25 ~~generating an electromagnetic field, or may be provided with connectors or the like enabling the at least one means to be connected to an external power supply.~~

~~In some embodiments, the means for generating the electromagnetic field have a height that is no more than half the width or half the length of the charging area; in~~
30 ~~some embodiments, the height may be no more than 1/5 of the width or 1/5 of the length of the charging area.~~

The at least one electrical conductor in the secondary device may be wound about a core that serves to concentrate flux therein. In particular, the core (where provided) may offer a path of least resistance to flux lines of the electromagnetic field generated by the primary unit. The core may be amorphous magnetically permeable material. In some embodiments, there is no need for an amorphous core.

Where an amorphous core is provided, it is preferred that the amorphous magnetic material is a non-annealed or substantially as-cast state. The material may be at least 70% non-annealed, or preferably at least 90% non-annealed. This is because annealing tends to make amorphous magnetic materials brittle, which is disadvantageous when contained in a device, such as a mobile phone, which may be subjected to rough treatment, for example by being accidentally dropped. In a particularly preferred embodiment, the amorphous magnetic material is provided in the form of a flexible ribbon, which may comprise one or more layers of one or more of the same or different amorphous magnetic materials. Suitable materials include alloys which may contain iron, boron and silicon or other suitable materials. The alloy is melted and then cooled so rapidly ("quenched") that there is no time for it to crystallise as it solidifies, thus leaving the alloy in a glass-like amorphous state. Suitable materials include Metglas® 2714A and like materials. Permalloy or mumetal or the like may also be used.

The core in the secondary device, where provided, is preferably a high magnetic permeability core. The relative permeability of this core is preferably at least 100, even more preferably at least 500, and most preferably at least 1000, with magnitudes of at least 10,000 or 100,000 being particularly advantageous.

The at least one means for generating an electromagnetic field may be a coil, for example in the form of a length of wire or a printed strip, or may be in the form of a conductive plate of appropriate configuration, or may comprise any appropriate arrangement of conductors. A preferred material is copper, although other conductive materials, generally metals, may be used as appropriate. It is to be understood that the term "coil" is here intended to encompass any appropriate

electrical conductor forming an electrical circuit through which current may flow and thus generate an electromagnetic field. In particular, the “coil” need not be wound about a core or former or the like, but may be a simple or complex loop or equivalent structure.

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Preferably, the charging area of the primary unit is large enough to accommodate the conductor and/or core of the secondary device in a plurality of orientations thereof. In a particularly preferred embodiment, the charging area is large enough to accommodate the conductor and/or core of the secondary device in any orientation thereof. In this way, power transfer from the primary unit to the secondary device may be achieved without having to align the conductor and/or core of the secondary device in any particular direction when placing the secondary device on the charging surface of the primary unit.

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15 The substantially laminar charging surface of the primary unit may be substantially planar, or may be curved or otherwise configured to fit into a predetermined space, such as a glove compartment of a car dashboard or the like. It is particularly preferred that the means for generating an electromagnetic field does not project or protrude above or beyond the charging surface.

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A key feature of the means for generating an electromagnetic field in the primary unit is that electromagnetic field lines generated by the means, measured when the primary unit is effectively in magnetic isolation (i.e. when no secondary device is present on or in proximity to the charging surface), are distributed in two dimensions over the at least one charging area and subtend an angle of 45° or less to the charging area in proximity thereto (for example, less than the height or width of the charging area) and over any quarter length part of the charging area measured in a direction generally parallel to that of the field lines. The measurement of the field lines in this connection is to be understood as a measurement of the field lines when averaged over the quarter length of the charging area, rather than an instantaneous point measurement. In some embodiments, the field lines subtend an angle of 30° or less, and in some embodiments are substantially parallel to at least a central part of the

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charging area in question. This is in stark contrast to prior art systems, where the field lines tend to be substantially perpendicular to a surface of a primary unit. By generating electromagnetic fields that are more or less parallel to or at least have a significant resolved component parallel to the charging area, it is possible to control the field so as to cause angular variations thereof, in or parallel to the plane of the charging area, that help to avoid any stationary nulls in the electromagnetic field that would otherwise reduce charging efficiency in particular orientations of the secondary device on the charging surface. The direction of the field lines may be rotated through a complete or partial circle, in one or both directions. Alternatively, the direction may be caused to “wobble” or fluctuate, or may be switched between two or more directions. In more complex configurations, the direction of the field lines may vary as a Lissajous pattern or the like.

In some embodiments, the field lines may be substantially parallel to each other over any given charging area, or at least have resolved components in or parallel to the plane of the charging area that are substantially parallel to each other at any given moment in time.

It is to be appreciated that one means for generating an electromagnetic field may serve to provide a field for more than one charging area; also that more than one means may serve to provide a field for just one charging area. In other words, there need not be a one-to-one correspondence of means for generating electromagnetic fields and charging areas.

The secondary device may adopt a substantially flat form factor with a core thickness of 2mm or less. Using a material such as one or more amorphous metal sheets, it is possible to have core thickness down to 1mm or less for applications where size and weight is important. See Figure 7a.

In a preferred embodiment, the primary unit may include a pair of conductors having adjacent coplanar windings which have mutually substantially parallel linear sections arranged so as to produce a substantially uniform electromagnetic field extending

generally parallel to or subtending an angle of 45° or less to the plane of the windings but substantially at right angles to the parallel sections;

5 The windings in this embodiment may be formed in a generally spiral shape, comprising a series of turns having substantially parallel straight sections;

Advantageously, the primary unit may include first and second pairs of conductors which are superimposed in substantially parallel planes with the substantially parallel linear sections of the first pair arranged generally at right angles to the substantially parallel linear sections of the second pair, and further comprising a driving circuit
10 which is arranged to drive them in such a way as to generate a resultant field which rotates in a plane substantially parallel to the planes of the windings;

According to a fifth aspect of the present invention, there is provided a system for
15 transferring power in a contactless manner consisting of:

- a primary unit consisting of at least one electrical coil whereby each coil features at least one active area whereby two or more conductors are substantially distributed over this area in such a fashion that it is possible for a secondary device to be placed in proximity to a part of this active area
20 where the net instantaneous current flow in a particular direction is substantially non-zero;

- at least one secondary device consisting of conductors wound around a high permeability core in such a fashion that it is possible for it to be placed in proximity to an area of the surface of the primary unit where the net instantaneous current flow is substantially non-zero;
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whereby the at least one secondary device is capable of receiving power by means of electromagnetic induction when the central axis of the winding is in proximity to the active area of the primary unit, is substantially not perpendicular to the plane of the active area of primary unit and is substantially not parallel to the conductors in the
30 active area of at least one of the coils of the primary unit.

Where the secondary device comprises an inductively-rechargeable battery or cell, the battery or cell may have a primary axis and be capable of being recharged by an alternating field flowing in the primary axis of the battery or cell, the battery or cell consisting of:

- 5 • an enclosure and external electrical connections similar in dimensions to industry standard batteries or cells
- an energy storage means
- an optional flux concentrating means
- 10 • a power receiving means
- a means of converting the received power to a form suitable for delivery to outside the cell through the external electrical connections, or to recharge the energy storage means, or both.

The proposed invention is a significant departure from the design of conventional inductive power transfer systems. The difference between conventional systems and the proposed system is best illustrated by looking at their respective magnetic flux line patterns. (See Figure 2a and 4)

- 20 • ~~Conventional System: In a conventional system (See Figure 2a), there is typically a planar primary coil which generates a magnetic field with flux lines coming out of the plane in a perpendicular fashion. The secondary device has typically a round or square coil that encircles some or all of these flux lines.~~
- 25 • ~~Proposed system: In the proposed system, the magnetic field travels substantially horizontally across the surface of the plane (see Figure 4) instead of directly out of the plane as illustrated in Figure 2a. The secondary device hence may have an elongated winding wound around a magnetic core. See Figure 7a and 7b. When the secondary device is placed on the primary unit, the flux lines would be attracted to travel through the magnetic core of the secondary device because it is the lowest reluctance path. This causes the secondary device and the primary unit to be coupled effectively. The~~
- 30

secondary-core and winding may be substantially flattened to form a very thin component.

5 In describing the invention, specific terminology will be resorted to for the sake of clarity. However, it is not intended that the invention be limited to the specific terms so selected and it is to be understood that each specific term includes all technical equivalents which operate in a similar manner to accomplish a similar purpose.

10 It is to be understood that the term "charging area" used in this patent application may refer to the area of the at least one means for generating a field (e.g. one or more conductors in the form of a coil) or an area formed by a combination of primary conductors where the secondary device can couple flux effectively. Some embodiments of this are shown in Figures 6a to 6l and 9e as component 740. A feature of a "charging area" is a distribution of conductors over a significant area of
15 the primary unit configured such that it is possible for the at least one means for generating a field to be driven to achieve an instantaneous net flow of flux in one direction. A primary unit may have more than one charging area. One charging area is distinct from another charging area when flux cannot be effectively coupled by the secondary device (such as those shown in Figure 7a) in any rotation at the boundary.

20 It is to be understood that the term "coil" used in this patent refers to all conductor configurations which feature a charging area as described above. This includes windings of wire or printed tracks or a plane as shown in Figure 8e. The conductors may be made of copper, gold, alloys or any other appropriate material.

25 The present application refers to the rotation of a secondary device in several places. It is to be clarified here that if a secondary device is rotated, the axis of rotation being referred to is the one perpendicular to the plane of the charging area.

30 This radical change in design overcomes a number of drawbacks of conventional systems. The benefits of the proposed invention include:

- ~~No need for accurate alignment: The secondary device can be placed anywhere on a charging area of the primary unit;~~
- 5 • ~~Uniform coupling: In the proposed invention, the coupling between the primary unit and secondary device is much more uniform over the charging area compared to a conventional primary and secondary coil. In a conventional large coil system (see Figure 2a), the field strength dips to a minimum at the centre of the coil, in the plane of the coil (see Figure 2b). This implies that if sufficient power is to be effectively transferred at the centre, the field strength at the minimum has to be above a certain threshold. The field strength at the maximum will then be excessively higher than the required threshold and this may cause undesirable effects.~~
- 10 • ~~Universality: a number of different secondary devices, even those having different power requirements, can be placed within charging areas on the charging surface of the primary unit to receive power simultaneously;~~
- 15 • ~~Increased coupling efficiency: Optional high permeability magnetic material present in the secondary device increases the induced flux significantly by offering a low reluctance path. This can significantly increase the power transfer.~~
- 20 • ~~Desirable form factor for secondary device: The geometry of the system allows thin sheets of magnetic material (such as amorphous metal ribbons) to be used. This means that secondary devices can have the form factor of a thin sheet, making it suitable to be incorporated at the back of mobile phones and other electronic devices. If magnetic material was to be used in the centre of conventional coils, it is likely to increase the bulkiness of the secondary device.~~
- 25 • ~~Minimised field leakage: When one or more secondary devices are present in the charging area of the primary unit, it is possible to use magnetic material in~~
- 30

such a way that more than half of the magnetic circuit is low-reluctance magnetic material (see figure 4d). This means that more flux flows for a given magneto-motive force (mmf). As the induced voltage is proportional to the rate of change of flux linked, this will increase the power transfer to the secondary device. The fewer and shorter the air-gaps are in the magnetic circuit, the less the field will fringe, the closer the flux is kept to the surface of the primary unit and hence leakage is minimized.

- Cost effectiveness: Unlike the multiple-coil design, this solution requires a much simpler control system and fewer components;
- Free axial rotation of secondary device: If the secondary device is thin or optionally even cylindrical (see Figure 10), it may be constructed such that it continues to couple well to the flux regardless of its rotation about its longest axis. This may in particular be an advantage if the secondary device is a battery cell fitted within another device, when its axial rotation may be difficult to control.
- The magnetic core in the secondary device may be located near other parallel planes of metal within or near the device, for example a copper printed circuit board or aluminium cover. In this case, the performance of embodiments of the present invention is significantly better than that of a conventional core-wound coil because the field lines through a conventional device coil will suffer flux exclusion if the coil is placed up against the metal plane (because the lines of flux must travel perpendicular to the plane of the coil). Since in embodiments of the present invention the lines of flux travel along the plane of the core, and therefore also of the metal plane, performance is improved. An additional benefit is that the magnetic core in a secondary device of embodiments of the present invention can act as a shield between the electromagnetic field generated by the primary unit and any items (e.g. electrical circuits, battery cells) on the other side of the magnetic core.

5 • Because its permeability is higher than that of air, the magnetic core of the secondary device of embodiments of the present invention acts to concentrate magnetic flux, thus capturing more flux than would otherwise flow through an equivalent cross-section of air. The size of the core's "shape factor" (the equivalent flux capturing sphere) is determined to a first-order approximation by the longest planar dimension of the core. Therefore if the core of the secondary device of embodiments of the present invention has planar dimensions with a significantly non-square aspect ratio, for example a 4:1 rectangle instead of a 1:1 square, it will capture proportionally more of any flux travelling parallel to the direction of its longest planar dimension. 10 Therefore if used in devices which have a constrained aspect ratio (for example a long thin device such as a headset or pen), a significant increase in performance will be experienced compared with that of a conventional coil of the same area.

15

The primary unit typically consists of the following components. (See Figure 5)

- 20 • Power supply: This power supply converts mains voltage into a lower voltage de supply. This is typically a conventional transformer or a switch-mode power supply;
- 25 • Control unit: The control unit serves the function of maintaining the resonance of the circuit given that the inductance of the means for generating a field changes with the presence of secondary devices. To enable this function, the control unit may be coupled to a sensing unit which feeds back the current status of the circuit. It may also be coupled to a library of capacitors which may be switched in and out as required. If the means for generating a field requires more than one driving circuit, the control unit may also coordinate the parameters such as the phase difference or on/off times of 30 different driving circuits such that the desired effect is achieved. It is also possible for the Q (quality factor) of the system to be designed to function

over a range of inductances such that a need for the above control system is eliminated;

• Driving circuit: The driving unit is controlled by the control unit and drives a changing current through the means for generating a field or a component of the means. More than one driving circuit may be present depending on the number of independent components in the means;

• Means for generating an electromagnetic field: The means uses current supplied from the driving circuits to generate electromagnetic fields of pre-defined shapes and intensities. The exact configuration of the means defines the shape and intensity of the field generated. The means may include magnetic material to act as flux guides and also one or more independently driven components (windings), together forming the charging area. A number of embodiment designs are possible and examples are shown in Figures 6;

• Sensing unit: The sensing unit retrieves and sends relevant data to the control unit for interpretation.

The secondary device typically consists of the following components, as shown in Figure 5:

• Magnetic unit: the magnetic unit converts the energy stored in the magnetic field generated by the primary unit back into electrical energy. This is typically implemented by means of a winding wound around a highly permeable magnetic core. The largest dimension of the core typically coincides with the central axis of the winding.

• Conversion unit: the conversion unit converts the fluctuating current received from the magnetic unit into a form that is useful to the device that it is coupled to. For example, the conversion unit may convert the fluctuating

current into an unregulated dc supply by means of a full-wave bridge rectifier and smoothing capacitor. In other cases, the conversion unit may be coupled to a heating element or a battery charger. There is also typically a capacitor present either in parallel or in series with the magnetic unit to form a resonant circuit at the operating frequency of the primary unit.

In typical operation, one or more secondary devices are placed on top of the charging surface of the primary unit. The flux flows through the at least one conductor and/or core of the secondary devices present and current is induced. Depending on the configuration of the means for generating a field in the primary unit, the rotational orientation of the secondary device may affect the amount of flux coupled.

The primary unit

The primary unit may exist in many different forms, for example:

- As a flat platform or pad which can sit on top of tables and other flat surfaces;
- Built in to furniture such as desks, tables, counters, chairs, bookcases etc. such that the primary unit may not be visible;
- As part of an enclosure such as a drawer, a box, a glove compartment of a car, a container for power tools;
- As a flat platform or pad which can be attached to a wall and used vertically.

The primary unit may be powered from different sources, for example:

- A mains AC power outlet
- A vehicle lighter socket
- Batteries
- Fuel Cells
- Solar Panel
- Human power

The primary unit may be small enough such that only one secondary device may be accommodated on the charging surface in a single charging area, or may be large

~~enough to accommodate many secondary devices simultaneously, sometimes in different charging areas.~~

~~The means for generating a field in the primary unit may be driven at mains frequency (50Hz or 60Hz) or at some higher frequency;~~

~~The sensing unit of the primary unit may sense the presence of secondary devices, the number of secondary devices present and even the presence of other magnetic material which is not part of a secondary device. This information may be used to control the current being delivered to the field-generating means of the primary unit;~~

~~The primary unit and/or the secondary device may be substantially waterproof or explosion-proof;~~

~~The primary unit and/or the secondary device may be hermetically sealed to standards such as IP66.~~

~~The primary unit may incorporate visual indicators (for example, but not limited to, light emitting devices, such as light emitting diodes, electrophosphorescent displays, light emitting polymers, or light reflecting devices, such as liquid crystal displays or MITs electronic paper) to indicate the current state of the primary unit, the presence of secondary devices or the number of secondary devices present or any combination of the above;~~

25 The means for generating an electromagnetic field

~~The field-generating means as referred to in this application includes all configurations of conductors where:~~

- ~~• The conductors are substantially distributed in the plane and;~~
- ~~• Substantial areas of the plane exist where there is a non-zero net instantaneous current flow. These are areas on which, given the correct orientation, the secondary devices will couple effectively and receive power. (See Figure 6)~~

- The conductors are capable of generating an electromagnetic field where the field lines subtend an angle of 45° or less or are substantially parallel to a substantial area of the plane.

5 Figures 6 illustrate some possibilities for such a primary conductor. Although most of the configurations are in fact coil windings, it is to be appreciated that the same effect can also be achieved with conductor planes which are not typically considered to be coils (See Figure 6e). These drawings are typical examples and are non-exhaustive. These conductors or coils may be used in combination such that the
10 secondary device can couple effectively in all rotations whilst on the charging area(s) of the primary unit.

Magnetic Material

It is possible to use magnetic materials in the primary unit to enhance performance.

15 •—Magnetic material may be placed below one or more charging areas or the entire charging surface such that there is also a low reluctance path on the underside of the conductors for the flux to complete its path. According to theory, an analogy can be drawn between magnetic circuits and electrical circuits. Voltage is analogous to magneto motive force (mmf), resistance is
20 analogous to reluctance and current is analogous to flux. From this, it can be seen that for a given mmf, flux flow will increase if the reluctance of the path is decreased. By providing magnetic material to the underside of the charging area, the reluctance of the magnetic circuit is essentially decreased. This substantially increases the flux linked by the secondary device and
25 ultimately increases the power transferred. Figure 4d illustrates a sheet of magnetic material placed underneath the charging area and the resulting magnetic circuit.

30 •—Magnetic material may also be placed above the charging surface and/or charging area(s) and below the secondary devices to act as a flux guide. This flux guide performs two functions: Firstly, the reluctance of the whole magnetic circuit is further decreased allowing more flux to flow. Secondly, it

provides a low-reluctance path along the top surface of the charging area(s) so the flux lines will flow through these flux guides in favour of flowing through the air. Hence this has the effect of containing the field close to the charging surface of the primary unit instead of in the air. The magnetic material used for flux guides may be strategically or deliberately chosen to have different magnetic properties to the magnetic core (where provided) of the secondary device. For example, a material with lower permeability and higher saturation may be chosen. High saturation means that the material can carry more flux and the lower permeability means that when a secondary device is in proximity, a significant amount of flux would then choose to travel through the secondary device in favour of the flux guide. (See Figures 8)

- In some configurations of the primary unit field-generating means, there may be conductors present that do not form part of the charging area, such as the component marked 745 in Figure 6a and 6b. In such cases, one may wish to use magnetic material to shield the effects of these conductors.

- Examples of some materials which may be used include but are not limited to: amorphous metal (metallic glass alloys such as MetGlas™), mesh of wires made of magnetic material, steel, ferrite cores, mumetal and permalloy.

The Secondary device

The secondary device may take a variety of shapes and forms. Generally, in order for good flux linkage, a central axis of the conductor (for example, a coil winding) should be substantially non-perpendicular to the charging area(s).

- The secondary device may be in the shape of a flattened winding. (See Figure 7a) The magnetic core inside can consist of sheets of magnetic material such as amorphous metals. This geometry allows the secondary device to be incorporated at the back of electronic devices such as mobile phones, personal digital assistants and laptops without adding bulk to the device.

- The secondary device may be in the shape of a long cylinder. A long cylindrical core could be wound with conductors (See Figure 7b);
 - The secondary device may be an object with magnetic material wrapped around it. An example is a standard sized (AA, AAA, C, D) or other sized/shaped (e.g. dedicated/customised for particular applications) rechargeable battery cell with for example magnetic material wrapped around the cylinder and windings around the cylindrical body;
 - The secondary device may be a combination of two or more of the above.
- The above embodiments may even be combined with a conventional coil.

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The following non-exhaustive list illustrates some examples of objects that can be coupled to a secondary device to receive power. Possibilities are not limited to those described below:

- A mobile communication device, for example a radio, mobile telephone or walkie-talkie;
- A portable computing device, for example a personal digital assistant or palmtop or laptop computer;
- Portable entertainment devices, for example a music player, games console or toy;
- Personal care items, for example a toothbrush, shaver, hair curler, hair rollers;
- A portable imaging device, for example a video camcorder or a camera;
- Containers of contents that may require heating, for example coffee mugs, plates, cooking pots, nail polish and cosmetic containers;
- Consumer devices, for example torches, clocks and fans;
- Power tools, for example cordless drills and screwdrivers;
- Wireless peripheral devices, for example wireless computer mouse, keyboard and headset;
- Time keeping devices, for example clock, wrist watch, stop watch and alarm clock;
- A battery pack for insertion into any of the above;
- A standard sized battery cell.

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In the case of unintelligent secondary devices such as a battery cell, some sophisticated charge control means may also be necessary to meter inductive power to the cell and to deal with situations where multiple cells in a device have different charge states. Furthermore, it becomes more important for the primary unit to be able to indicate a "charged" condition, since the secondary cell or battery may not be easily visible when located inside another electrical device.

A possible system comprising an inductively rechargeable battery or cell and a primary unit is shown in Figure 10. In addition to the freedom to place the battery 920 freely in (X,Y) and optionally rotate it in rZ, relative to the primary unit 910, the battery can also be rotated along its axis rA while continuing to receive power.

When a user inserts a battery into a portable device, it is not easy to ensure that it has any given axial rotation. Therefore, embodiments of the present invention are highly advantageous because they can ensure that the battery can receive power while in any random orientation about rA.

The battery or cell may include a flux concentrating means that may be arranged in a variety of ways:

1. As shown in Figure 11a, a cell 930 may be wrapped in a cylinder of flux-concentrating material 931, around which is wrapped a coil of wire 932.
 - a. The cylinder may be long or short relative to the length of the cell.
2. As shown in Figure 11b, a cell 930 may have a portion of flux-concentrating material 931 on its surface, around which is wrapped a coil of wire 932.
 - a. The portion may be conformed to the surface of the cell, or embedded within it.
 - b. Its area may be large or small relative to the circumference of the cell, and long or short relative to the length of the cell.
3. As shown in Figure 11c, a cell 930 may contain a portion of flux-concentrating material 931 within it, around which is wrapped a coil of wire 932.

- a. The portion may be substantially flat, cylindrical, rod-like, or any other shape.
- b. Its width may be large or small relative to the diameter of the cell
- c. Its length may be large or small relative to the length of the cell

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In any of these cases, the flux concentrator may be a functional part of the battery enclosure (for example, an outer zinc electrode) or the battery itself (for example, an inner electrode):

10 Issues relating to charging of secondary cells (e.g., AA rechargeable cells in situ within an appliance include:

- Terminal voltage could be higher than normal.
- Cells in series may behave strangely, particularly in situations where some cells are charged, others not.

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- Having to provide enough power to run the device and charge the cell.
- If fast charging is effected incorrectly, the cells may be damaged.

Accordingly, some sophisticated charge control means to meter inductive power to the appliance and the cell is advantageously provided. Furthermore, it becomes more
 20 important for the primary unit to be able to indicate a “charged” condition, since the secondary cell or battery may not be easily visible when located inside an electrical device.

A cell or battery enabled in this fashion may be charged whilst fitted in another
 25 device, by placing the device onto the primary unit, or whilst outside the device by placing the cell or battery directly onto the primary unit.

Batteries enabled in this fashion may be arranged in packs of cells as in typical devices (e.g. end to end or side by side), allowing a single pack to replace a set of
 30 cells.

Alternatively, the secondary device may consist of a flat “adapter” which fits over the batteries in a device, with thin electrodes which force down between the battery electrodes and the device contacts.

5 ***Rotating electromagnetic field***

In the coils such as those in Figure 6, 9a and 9b, the secondary devices will generally only couple effectively when the windings are placed substantially parallel to the direction of net current flow in the primary conductor as shown by the arrow 1. In some applications, one might require a primary unit which will transfer power
10 effectively to secondary devices regardless of their rotation as long as:

- the central axis of the secondary conductor is not perpendicular to the plane and;
- the secondary device is in close proximity to the primary unit

15 To enable this, it is possible to have two coils, for example one positioned on top of the other or one woven into or otherwise associated with the other, the second coil capable of generating a net current flow substantially perpendicular to the direction of the first coil at any point in the active area of the primary unit. These two coils may be driven alternately such that each is activated for a certain period of time.
20 Another possibility is to drive the two coils in quadrature such that a rotating magnetic dipole is generated in the plane. This is illustrated in Figure 9. This is also possible with other combinations of coil configurations.

Resonant circuits

25 It is known in the art to drive coils using parallel or series resonant circuits. In series resonant circuits for example, the impedance of the coil and the capacitor are equal and opposite at resonance, hence the total impedance of the circuit is minimised and a maximum current flows through the primary coil. The secondary device is typically also tuned to the operating frequency to maximise the induced voltage or
30 current.

In some systems like the electric toothbrush, it is common to have a circuit which is detuned when the secondary device is not present and tuned when the secondary device is in place. The magnetic material present in the secondary device shifts the self inductance of the primary unit and brings the circuit into resonance. In other
5 systems like passive radio tags, there is no magnetic material in the secondary device and hence does not affect the resonant frequency of the system. These tags are also typically small and used far from the primary unit such that even if magnetic material is present, the inductance of the primary is not significantly changed.

10 In the proposed system, this is not the case:

- High permeability magnetic material may be present in the secondary device and is used in close proximity to the primary unit;
- One or more secondary devices may be brought in close proximity to the primary unit simultaneously.

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This has the effect of shifting the inductance of the primary significantly and also to different levels depending on the number of secondary devices present on the pad. When the inductance of the primary unit is shifted, the capacitance required for the circuit to resonant at a particular frequency also changes. There are three methods
20 for keeping the circuit at resonance:

- By means of a control system to dynamically change the operating frequency;
- By means of a control system to dynamically change the capacitance such that resonance is achieved at the predefined frequency;
- By means of a low Q system where the system remains in resonance over a
25 range of inductances.

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The problem with changing the operating frequency is that the secondary devices are typically configured to resonate at a predefined frequency. If the operating frequency changes, the secondary device would be detuned. To overcome this
30 problem, it is possible to change the capacitance instead of the operating frequency. The secondary devices can be designed such that each additional device placed in proximity to the primary unit will shift the inductance to a quantised level such that

an appropriate capacitor can be switched in to make the circuit resonate at a predetermined frequency. Because of this shift in resonant frequency, the number of devices on the charging surface can be detected and the primary unit can also sense when something is brought near or taken away from the charging surface. If a magnetically permeable object other than a valid secondary device is placed in the vicinity of the charging surface, it is unlikely to shift the system to the predefined quantised level. In such circumstances, the system could automatically detune and reduce the current flowing into the coil.

For a better understanding of the present invention and to show how it may be carried into effect, reference shall now be made, by way of example only, to the accompanying drawings, in which:

FIGURE 1 shows the magnetic design of typical prior art contact less power transfer systems which require accurate alignment of the primary unit and secondary device;

FIGURE 2a shows the magnetic design of another typical prior art contact less power transfer system which involves a large coil in the primary unit;

FIGURE 2b shows the non uniform field distribution inside the large coil at 5mm distance from the plane of the coil, exhibiting a minimum in the centre;

FIGURE 3 shows a multiple coil system where each coil is independently driven such that a localised field can be generated.

FIGURE 4a shows an embodiment of the proposed system which demonstrates a substantial departure from prior art with no secondary devices present;

FIGURE 4b shows an embodiment of the proposed system with two secondary devices present;

FIGURE 4c shows a cross section of the active area of the primary unit and the

contour lines of the magnetic flux density generated by the conductors;

FIGURE 4d shows the magnetic circuit for this particular embodiment of the proposed invention;

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FIGURE 5 shows a schematic drawing of an embodiment of the primary unit and the secondary device;

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FIGURE 6a to 6l show some alternative embodiment designs for the field generating means or a component of the field generating means of the primary unit;

FIGURES 7a and 7b show some possible designs for the magnetic unit of the secondary device;

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FIGURES 8 shows the effect of flux guides (the thickness of the flux guide has been exaggerated for clarity);

20

FIGURE 8a shows that without flux guides, the field tends to fringe into the air directly above the active area;

FIGURE 8b shows the direction of current flow in the conductors in this particular embodiment;

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FIGURE 8c shows that the flux is contained within the flux guides when magnetic material is placed on top of the charging area;

FIGURE 8d shows a secondary device on top of the primary unit;

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FIGURE 8e shows a cross section of the primary unit without any secondary devices;

FIGURE 8f shows a cross section of the primary unit with a secondary device on top and demonstrates the effect of using a secondary core with higher permeability than

the flux guide.

FIGURE 9a shows a particular coil arrangement with a net instantaneous current flow shown by the direction of the arrow;

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FIGURE 9b shows a similar coil arrangement to FIGURE 9a except rotated by 90 degrees;

FIGURE 9c shows the charging area of the primary unit if the coil of FIGURE 9a is placed on top of FIGURE 9b. If the coil in FIGURE 9a is driven in quadrature to FIGURE 9b, the effect is a rotating magnetic dipole shown here;

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FIGURE 10 shows the case where the secondary device has an axial degree of rotation;

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FIGURE 11 shows various arrangements of secondary devices with axial degrees of rotation;

FIGURE 12a and FIGURE 12b show another embodiment of the type of coil arrangement shown in FIGURE 9a and FIGURE 9b; and

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FIGURE 13 shows a simple embodiment of driving unit electronics;

Referring firstly to Figure 1, there is shown two examples of prior art contact less power transfer systems which both require accurate alignment of a primary unit and a secondary device. This embodiment is typically used in electric toothbrush or mobile phone chargers.

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Figure 1a shows a primary magnetic unit 100 and a secondary magnetic unit 200. On the primary side, a coil 110 is wound around a magnetic core 120 such as ferrite. Similarly, the secondary side consists of a coil 210 wound around another magnetic core 220. In operation, an alternating current flows in to the primary coil 110 and

30

generates lines of flux **1**. When a secondary magnetic unit **200** is placed such that it is axially aligned with the primary magnetic unit **100**, the flux **1** will couple from the primary into the secondary, inducing a voltage across the secondary coil **210**.

5 Figure 1b shows a split transformer. The primary magnetic unit **300** consists of a U-shaped core **320** with a coil **310** wound around it. When alternating current flows into the primary coil **310**, changing lines of flux are generated **1**. The secondary magnetic unit **400** consists of a second U-shaped core **420** with another coil **410** wound around it. When the secondary magnetic unit **400** is placed on the primary
10 magnetic unit **300** such that the arms of the two U-shaped cores are in alignment, the flux will couple effectively into the core of the secondary **420** and induce voltage across the secondary coil **410**.

Figure 2a is another embodiment of prior art inductive systems typically used in
15 powering radio frequency passive tags. The primary typically consists of a coil **510** covering a large area. Multiple secondary devices **520** will have voltage induced therein when they are within the area encircled by the primary coil **510**. This system does not require the secondary coil **520** to be accurately aligned with the primary coil **510**. Figure 2b shows a graph of the magnitude of magnetic flux intensity across the
20 area encircled by the primary coil **510** at 5mm above the plane of the primary coil. It shows a non-uniform field, which exhibits a minimum **530** at the centre of the primary coil **510**.

Figure 3 is another embodiment of a prior art inductive system wherein a multiple
25 coil array is used. The primary magnetic unit **600** consists of an array of coils including coils **611**, **612**, **613**. The secondary magnetic unit **700** may consist of a coil **710**. When the secondary magnetic unit **700** is in proximity to some coils in the primary magnetic unit **600**, the coils **611**, **612** are activated while other coils such as **613** remain inactive. The activated coils **611**, **612** generate flux, some of which will
30 couple into the secondary magnetic unit **700**.

Figure 4 shows an embodiment of the proposed invention. Figure 4a shows a

primary-coil 710 wound or printed in such a fashion that there is a net instantaneous current flow within the active area 740. For example, if a dc current flows through the primary-coil 710, the conductors in the active area 740 would all have current flowing in the same direction. Current flowing through the primary-coil 710 generates flux 1. A layer of magnetic material 730 is present beneath the charging area to provide a return path for the flux. Figure 4b shows the same primary magnetic unit as shown in Figure 4a with two secondary devices 800 present. When the secondary devices 800 are placed in the correct orientation on top of the charging area 740 of the primary magnetic unit, the flux 1 will flow through the magnetic core of the secondary devices 800 instead of flowing through the air. The flux 1 flowing through the secondary core would hence induce current in the secondary coil.

Figure 4c shows some contour lines for the flux density of the magnetic field generated by the conductors 711 in the charging area 740 of the primary magnetic unit. There is a layer of magnetic material 730 beneath the conductors to provide a low reluctance return path for the flux.

Figure 4d shows a cross section of the charging area 740 of the primary magnetic unit. A possible path for the magnetic circuit is shown. The magnetic material 730 provides a low reluctance path for the circuit and also the magnetic core 820 of the secondary magnetic device 800 also provides a low reluctance path. This minimizes the distance the flux has to travel through the air and hence minimizes leakage.

Figure 5 shows a schematic drawing of an embodiment of the whole system of the proposed invention. In this embodiment, the primary unit consists of a power supply 760, a control unit 770, a sensing unit 780 and an electromagnetic unit 790. The power supply 760 converts the mains (or other sources of power) into a dc supply at an appropriate voltage for the system. The control unit 770 controls the driving unit 790 which drives the magnetic unit 700. In this embodiment, the magnetic unit consists of two independently driven components, coil 1 and coil 2, arranged such that the conductors in the charging area of coil 1 would be perpendicular to the conductors in the charging area of coil 2. When the primary unit is activated, the

control unit causes a 90-degree phase shift between the alternating current that flows through coil 1 and coil 2. This creates a rotating magnetic dipole on the surface of the primary magnetic unit 700 such that a secondary device is able to receive power regardless of its rotational orientation (See Figure 9). In standby mode where no
5 secondary devices are present, the primary unit is detuned and current flow into the magnetic unit 700 is minimised. When a secondary device is placed on top of the charging area of the primary unit, the inductance of the primary magnetic unit 700 is changed. This brings the primary circuit into resonance and the current flow is maximised. When there are two secondary devices present on the primary unit, the
10 inductance is changed to yet another level and the primary circuit is again detuned. At this point, the control unit 770 uses feedback from the sensing unit 780 to switch another capacitor into the circuit such that it is tuned again and current flow is maximised. In this embodiment, the secondary devices are of a standard size and a maximum of six standard sized devices can receive power from the primary unit simultaneously. Due to the standard sizes of the secondary devices, the change in
15 inductance due to the change in secondary devices in proximity is quantized to a number of predefined levels such that only a maximum of 6 capacitances is required to keep the system operating at resonance.

20 Figures 6a to 6l show a number of different embodiments for the coil component of the primary magnetic unit. These embodiments may be implemented as the only coil component of the primary magnetic unit, in which case the rotation of the secondary device is important to the power transfer. These embodiments may also be implemented in combination, not excluding embodiments which are not illustrated
25 here. For example, two coils illustrated in Figure 6a may be placed at 90 degrees to each other to form a single magnetic unit. In Figures 6a to 6e, the charging area 740 consists of a series of conductors with net current generally flowing in the same direction. In certain configurations, such as Figure 6c, there is no substantial linkage when the secondary device is placed directly over the centre of the coil and hence
30 power is not transferred. In Figure 6d, there is no substantial linkage when the secondary device is positioned in the gap between the two charging areas 740.

Figure 6f shows a specific coil configuration for the primary unit adapted to generate electromagnetic field lines substantially parallel to a surface of the primary unit within the charging area 740. Two primary windings 710, one on either side of the charging area 740, are formed about opposing arms of a generally rectangular flux guide 750 made out of a magnetic material, the primary windings 710 generating opposing electromagnetic fields. The flux guide 750 contains the electromagnetic fields and creates a magnetic dipole across the charging area 740 in the direction of the arrows indicated on the Figure. When a secondary device is placed in the charging area 740 in a predetermined orientation, a low reluctance path is created and flux flows through the secondary device, causing effective coupling and power transfer. It is to be appreciated that the flux guide 750 need not be continuous, and may in fact be formed as two opposed and non-linked horseshoe components.

Figure 6g shows another possible coil configuration for the primary unit, the coil configuration being adapted to generate electromagnetic field lines substantially parallel to the charging surface of the primary unit within the charging area 740. A primary winding 710 is wound around a magnetic core 750 which may be ferrite or some other suitable material. The charging area 740 includes a series of conductors with instantaneous net current generally flowing in the same direction. The coil configuration of Figure 6g is in fact capable of supporting or defining a charging area 740 on both upper and lower faces as shown in the drawing, and depending on the design of the primary unit, one or both of the charging areas may be made available to secondary devices.

Figure 6h shows a variation of the configuration of Figure 6g. Instead of the primary windings 710 being evenly spaced as in Figure 6g, the windings 710 are not evenly spaced. The spacing and variations therein can be selected or designed so as to provide improved uniformity of performance or field strength levels over the charging area 740.

Figure 6i shows an embodiment in which two primary windings 710 as shown in Figure 6g are located in a mutually orthogonal configuration so as to enable a

direction of the field lines to be dynamically switched or rotated to other orientations about the plane of the charging surface.

Figures 6j and 6k show additional two-coil configurations for the primary unit which
5 are not simple geometric shapes with substantially parallel conductors.

In Figure 6j, line 710 indicates one of a set of current-carrying conductors lying in the plane of the charging surface 600. The shape of the main conductor 710 is arbitrary and need not be a regular geometric figure—indeed, conductor 710 may
10 have straight and curved sections and may intersect with itself. One or more subsidiary conductors 719 are arranged alongside and generally parallel (at any given local point) to the main conductor 710 (only two subsidiary conductors 719 are shown here for clarity). Current flow in subsidiary conductors 719 will be in the same direction as in the main conductor 710. The subsidiary conductors 719 may be
15 connected in series or parallel so as to form a single coil arrangement.

In Figure 6k, a set of current-carrying conductors 720 (only some of which are shown for clarity) is arranged in the plane of the charging surface 600. A main conductor 710 is provided as in Figure 6j, and the conductors 720 are each arranged
20 so as to be locally orthogonal to the main conductor 710. The conductors 720 may be connected in series or parallel so as to form a single coil arrangement. If a first sinusoidal current is fed into the conductor 710, and a second sinusoidal current having a 90° phase shift relative to the first current is fed into the coil 720, then by
varying the relative proportions and signs of the two currents a direction of a
25 resultant electromagnetic field vector at most points on the charging area 740 will be seen to rotate through 360°.

Figure 6l shows yet another alternative arrangement in which the magnetic core 750 is in the shape of a round disc with a hole in the centre. The first set of current
30 carrying conductors 710 is arranged in a spiral shape on the surface of the round disc. The second set of conductors 720 is wound in a toroidal format through the centre of the disc and out to the perimeter in a radial fashion. These conductors can be driven

in such a way, for example with sinusoidal currents at quadrature, that when a secondary device is placed at any point inside the charging area 740 and rotated about an axis perpendicular to the charging area, no nulls are observed by the secondary device.

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Figure 7a and 7b are embodiments of the proposed secondary devices. A winding 810 is wound around a magnetic core 820. Two of these may be combined in a single secondary device, at right angles for example, such that the secondary device is able to effectively couple with the primary unit at all rotations. These may also be combined with standard coils, as the ones shown in Figure 2a 520 to eliminate dead spots.

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Figure 8 shows the effect of flux guides 750 positioned on top of the charging area. The thickness of the material has been exaggerated for the sake of clarity but in reality would be in the order of millimetres thick. The flux guides 750 will minimize leakage and contain the flux at the expense of reducing the amount of flux coupled to the secondary device. In Figure 8a, a primary magnetic unit is shown without flux guides 750. The field will tend to fringe into the air directly above the charging area. With flux guides 750, as shown in Figure 8b to 8f, the flux is contained within the plane of the material and leakage is minimised. In Figure 8e, when there is no secondary device 800 on top, the flux remains in the flux guide 750. In Figure 8f, when a secondary device 800 is present with a relatively more permeable material as the core, part of the flux will flow via the secondary device. The permeability of the flux guide 750 can be chosen such that it is higher than that of typical metals such as steel. When other materials such as steel, which are not part of secondary devices 800, are placed on top, most of the flux will remain in the flux guide 750 instead of travelling through the object. The flux guide 750 may not be a continuous layer of magnetic material but may have small air gaps in them to encourage more flux flow into the secondary device 800 when it is present.

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Figure 9 shows an embodiment of a primary unit whereby more than one coil is used. Figure 9a shows a coil 710 with a charging area 740 with current flow parallel to the

direction of the arrow 2. Figure 9b shows a similar coil arranged at 90 degrees to the one in Figure 9a. When these two coils are placed on top of each other such that the charging area 740 overlaps, the charging area will look like the illustration in Figure 9c. Such an embodiment would allow the secondary device to be at any rotation on top of the primary unit and couple effectively.

Figure 10 shows an embodiment where the secondary device has an axial degree of rotation, for example where it is, or is embedded within, a battery cell. In this embodiment the secondary device may be constructed such that it couples to the primary flux when in any axial rotation (rA) relative to the primary unit (910), as well as having the same degrees of freedom described above (i.e., translational (X,Y) and optionally rotational perpendicular to the plane of the primary (rZ)).

Figure 11a shows one arrangement where a rechargeable battery cell 930 is wrapped with an optional cylinder of flux concentrating material 931 which is itself wound with copper wire 932. The cylinder may be long or short relative to the length of the cell.

Figure 11b shows another arrangement where the flux concentrating material 931 covers only part of the surface of the cell 930, and has copper wire 932 wrapped around it (but not the cell). The material and wire may be conformed to the surface of the cell. Their area may be large or small relative to the circumference of the cell, and long or short relative to the length of the cell.

Figure 11c shows another arrangement where the flux concentrating material 931 is embedded within the cell 930 and has copper wire 932 wrapped around it. The material may be substantially flat, cylindrical, rod like, or any other shape, its width may be large or small relative to the diameter of the cell, and its length may be large or small relative to the length of the cell.

In any case shown in Figures 10 and 11, any flux-concentrating material may also be a functional part of the battery enclosure (for example, an outer zinc electrode) or the battery itself (for example, an inner electrode).

5 In any case shown in Figures 10 and 11, the power may be stored in a smaller standard cell (e.g. AAA size) fitted within the larger standard cell enclosure (e.g. AA).

Figure 12 shows an embodiment of a primary unit similar to that shown in Figure 9.
10 Figure 12a shows a coil generating a field in a direction horizontal to the page, Figure 12b shows another coil generating a field vertical to the page, and the two coils would be mounted in a substantially coplanar fashion, possibly with one above the other, or even intertwined in some fashion. The wire connections to each coil are shown 940 and the charging area is represented by the arrows 941.

15 Figure 13 shows a simple embodiment of the Driving Unit (790 of Figure 5). In this embodiment there is no Control Unit. The PIC processor 960 generates two 23.8kHz square waves 90 degrees out of phase with one another. These are amplified by components 961 and driven into two coil components 962, which are the same
20 magnetic units shown in Figure 12a and Figure 12b. Although the driving unit is providing square waves, the high resonant "Q" of the magnetic units shapes this into a sinusoidal waveform.

The preferred features of the invention are applicable to all aspects of the invention
25 and may be used in any possible combination.

Throughout the description and claims of this specification, the words "comprise" and "contain" and variations of the words, for example "comprising" and "comprises", mean "including but not limited to", and are not intended to (and do
30 not) exclude other components, integers, moieties, additives or steps.